CE 374 K – Hydrology

Infiltration

Daene C. McKinney

Porous Medium

• Groundwater

- All waters found beneath the ground surface
- Occupies pores (void space space not occupied by solid matter)

• Porous media

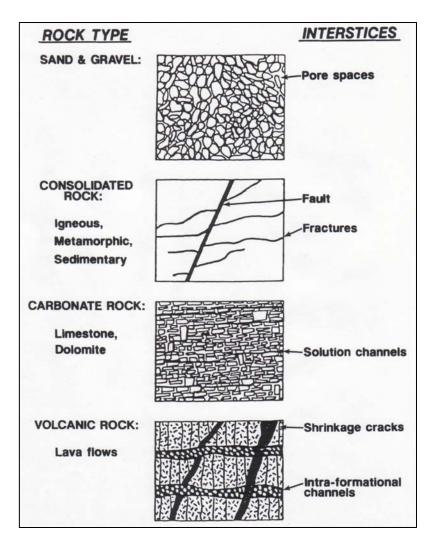
- Numerous pores of small size
- Pores contain fluids (e.g., water and air)
- Pores act as conduits for flow of fluids

• Type of rocks in a formation and their

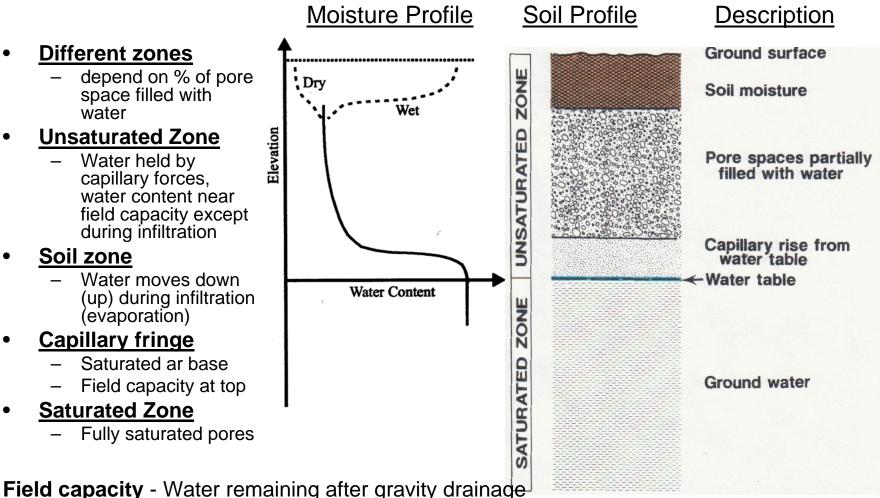
- Number, size, and arrangement of pores
- Affect the storage and flow through a formation.

• Pores shapes are irregular because

- differences in the minerals making up the rocks
- geologic processes experienced by them.



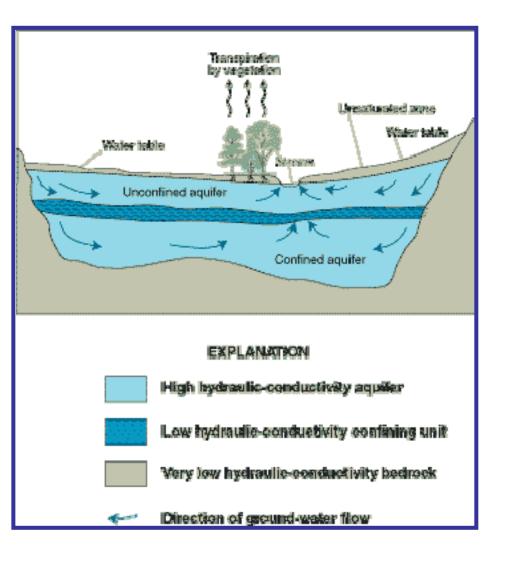
Distribution of Subsurface Water



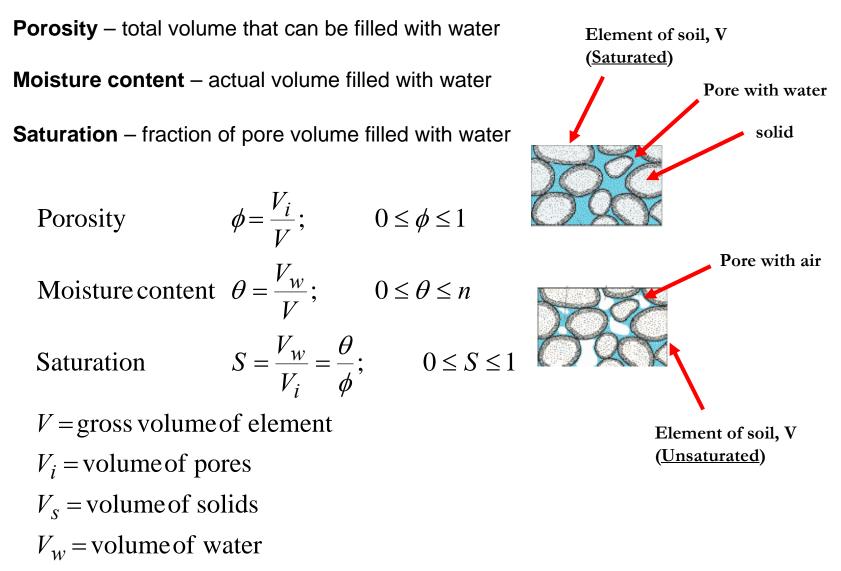
<u>**Wilting point</u></u> - Water remaining after gravity drainage <u>Wilting point**</u> - Water remaining after gravity drainage & evapotranspiration</u>

Aquifer Types

- Aquifer store & transmit
 - Unconsolidated deposits sand and gravel, sandstones etc.
- <u>Aquiclude</u> store, don't transmit
 - Clays and less shale
 - Impervious boundaries of aquifers
- <u>Aquitard</u> transmit don't store
 - Shales and less clay
 - Leaky confining layers of aquifers
- <u>Confined aquifer</u>
 - Under pressure
 - Bounded by impervious layers
- Unconfined aquifer
 - Phreatic aquifer, water table aquifer
 - Bounded above by water table
 - Atmospheric pressure at water table



Porosity



Aquifer Properties

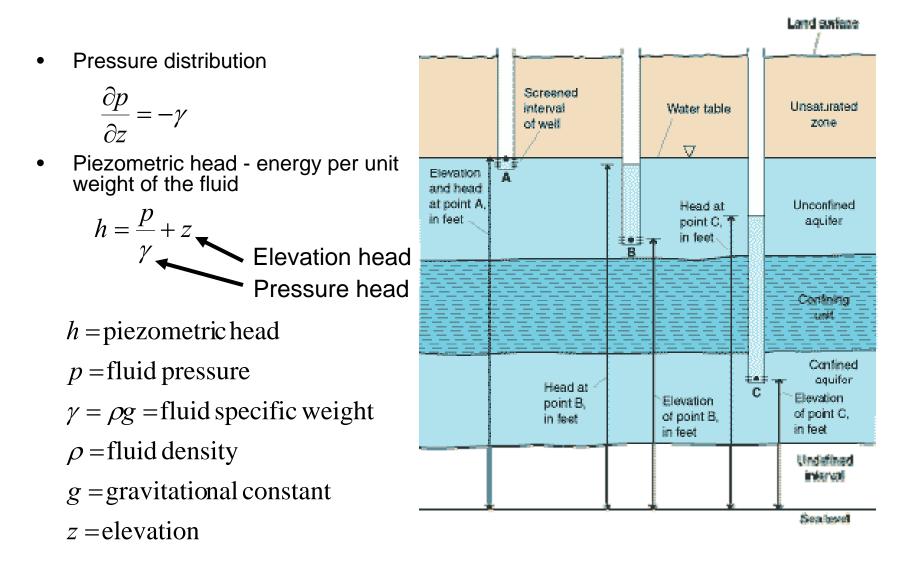
- <u>**Porosity**</u> (*n*)
 - Percent of total pore space occupied by voids

• <u>Hydraulic conductivity</u> (K)

- Ability of a formation to transmit water
- <u>Storativity</u> (S)
 - Ability of a formation to store water

Sedimentary Material	Porosity (%)
Peat Soil	60-80
Soils	50-60
Clay	45-55
Silt	40-50
Med. to Coarse Sand	35-40
Uniform Sand	30-40
Fine to Med Sand	30-35
Gravel	30-40
Gravel and Sand	30-35
Sandstone	10-20
Shale	1-10
Limestone	1-10

Piezometric Head





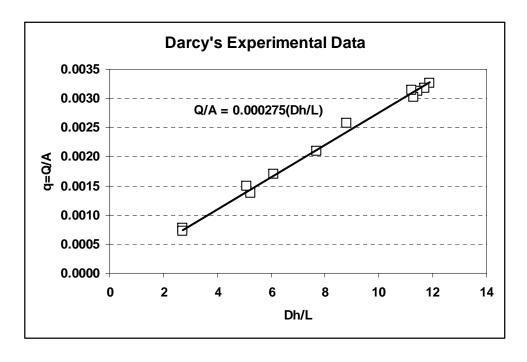
Dijon Fountain



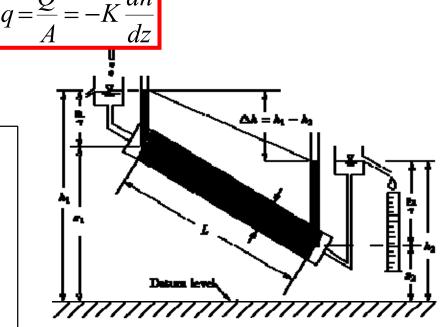
 Output is proportional to the head and inversely related to the length traversed







 $Q \propto A \frac{h_1 - h_2}{L}$



K = hydraulic conductivity q = Q/A = specific discharge

Continuity Equation

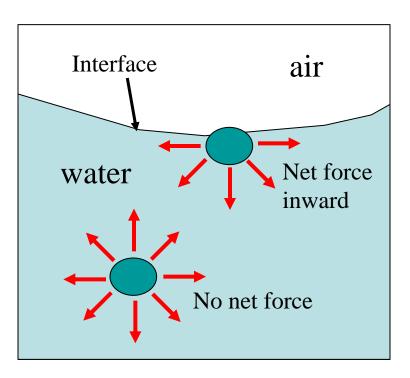
V = dxdydz = volume of element $V_w = \theta dxdydz = \text{volume of water}$ $\frac{d}{dt} \iiint_{CV} \rho_w d\forall + \iint_{CS} \rho_w \mathbf{V} \cdot \mathbf{dA} = 0$ $\rho_w dxdydz \frac{d\theta}{dt} + \rho_w dzdxdy \frac{\partial q}{\partial z} = 0$ $q_z = -K \frac{\partial h}{\partial z}$

$$\frac{\partial \theta}{\partial t} + \frac{\partial q}{\partial z} = 0$$

Continuity Equation

Surface Tension

- Below interface
 - forces act equally in all directions
- At interface
 - some forces are missing
 - pulls molecules down and together
 - like membrane exerting tension on the surface
- If interface is curved
 - higher pressure will exist on concave side
- Pressure increase
 - balanced by surface tension, σ
- $\sigma = 0.073 \text{ N/m} (@ 20^{\circ}\text{C})$



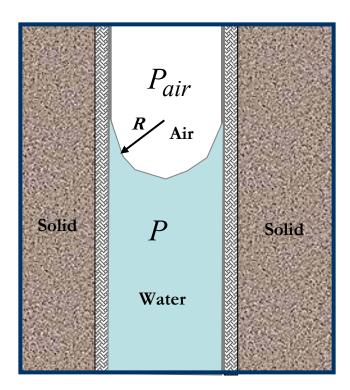
Capillary Action

- Capillary Pressure
 - Related to surface tension and size of pores

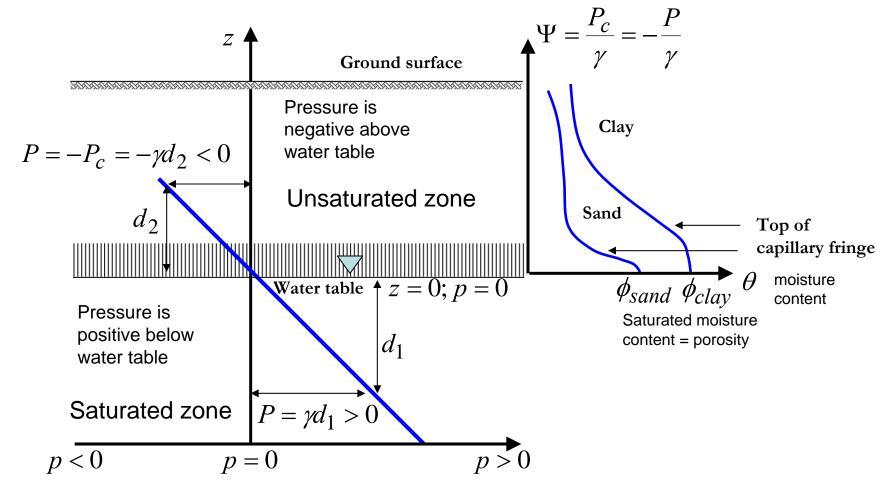
$$P_c = \frac{2\sigma}{R} = P_{air} - P$$
$$P_{air} = 0$$

$$P_c = -P$$

- Related to water content $P_c = P_c(\theta)$
- Suction Head $\Psi = \frac{P_c}{\gamma}$
- Total Head $h = \Psi + z$



Pressure Distribution in Subsurface



Richard's Equation

• Darcy's Law becomes

$$\begin{split} h &= \Psi + z \qquad \qquad q_z = -K \frac{\partial h}{\partial z} = -K \frac{\partial (\Psi + z)}{\partial z} = -\left(K \frac{\partial \Psi}{\partial \theta} \frac{\partial \theta}{\partial z} + K\right) \\ &= -\left(D \frac{\partial \theta}{\partial z} + K\right) \qquad \qquad D = K \frac{\partial \Psi}{\partial \theta} \end{split}$$

• Continuity becomes

$$\frac{\partial \theta}{\partial t} + \frac{\partial q}{\partial z} = 0$$

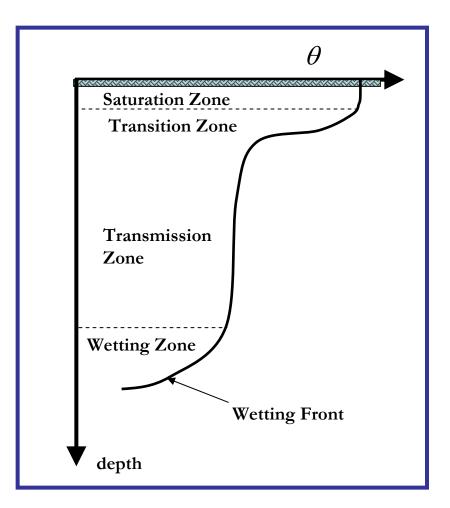
$$\frac{\partial \theta}{\partial t} = \frac{\partial}{\partial z} \left(D \frac{\partial \theta}{\partial z} + K \right)$$

Richard's Equation

Soil water diffusivity

Infiltration

- General
 - Process of water penetrating from ground into soil
 - Factors affecting
 - Condition of soil surface, vegetative cover, soil properties, hydraulic conductivity, antecedent soil moisture
 - Four zones
 - Saturated zone
 - Transmission zone
 - Wetting zone
 - Wetting front



Infiltration

- Infiltration rate
 - Rate at which water enters the soil at the surface f(t)
- Cumulative infiltration
 - Accumulated depth of water infiltrating during given time period

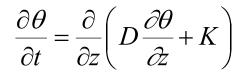
$$F(t) = \int_{0}^{t} f(\tau) d\tau$$
$$f(t) = \frac{dF(t)}{dt}$$

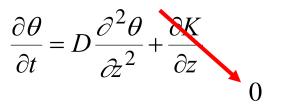
Infiltration Methods

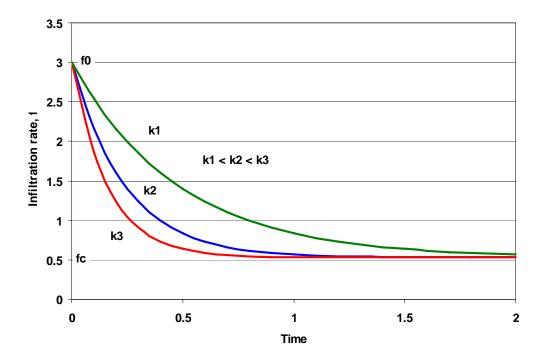
- Horton and Phillips
 - Infiltration models developed from
 - <u>approximate solutions</u> to <u>exact theory</u> (Richard's Equation)
- Green Ampt
 - Infiltration model developed from
 - <u>exact solution</u> to <u>approximate theory</u>

Hortonian Infiltration

- Recall Richard's Equation
 - Assume K and D are constants, not a function of θ or z
- Solve for moisture diffusion at surface







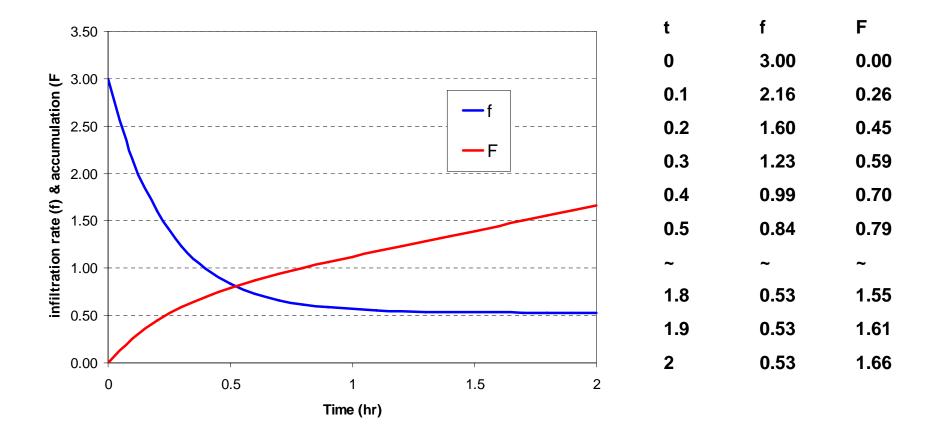
$$\frac{\partial \theta}{\partial t} = D \frac{\partial^2 \theta}{\partial z^2}$$

$$f(t) = f_{c} + (f_{0} - f_{c})e^{-kt}$$

Horton's Equation

$$F(t) = \int_{0}^{t} f(\tau) d\tau$$
 Trapezoid Rule

$$F(t_n) = \int_0^{t_n} f(\tau) d\tau \approx \frac{\Delta t}{2} (f_0 + 2f_1 + \dots + 2f_{n-1} + f_n) = \frac{\Delta t}{2} (f_0 + 2\sum_{i=1}^{n-1} f_i + f_n)$$



Philip's Equation

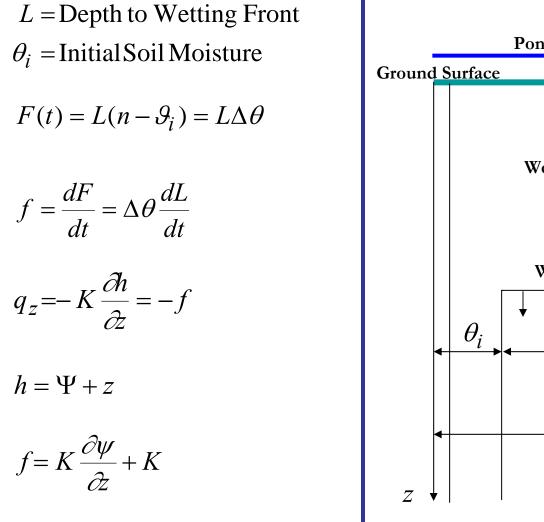
- Recall Richard's Equation
 - Assume K and D are functions of θ , not z
- Solution
 - Two terms represent effects of
 - Suction head
 - Gravity head
- S Sorptivity
 - Found from experiment

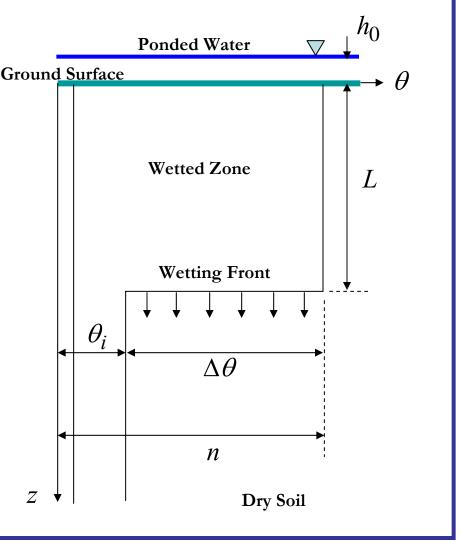
$$\frac{\partial \theta}{\partial t} = \frac{\partial}{\partial z} \left(D \frac{\partial \theta}{\partial z} + K \right)$$

$$f(t) = \frac{1}{2}S\sqrt{t} + Kt$$

Philip's Equation

Green – Ampt Infiltration

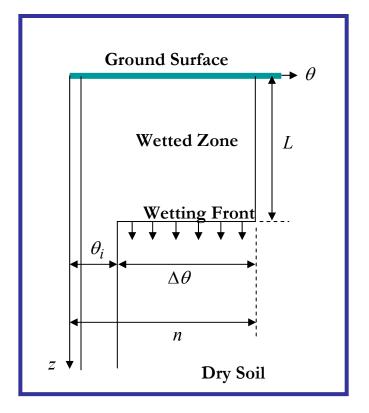




Green – Ampt Infiltration (Cont.)

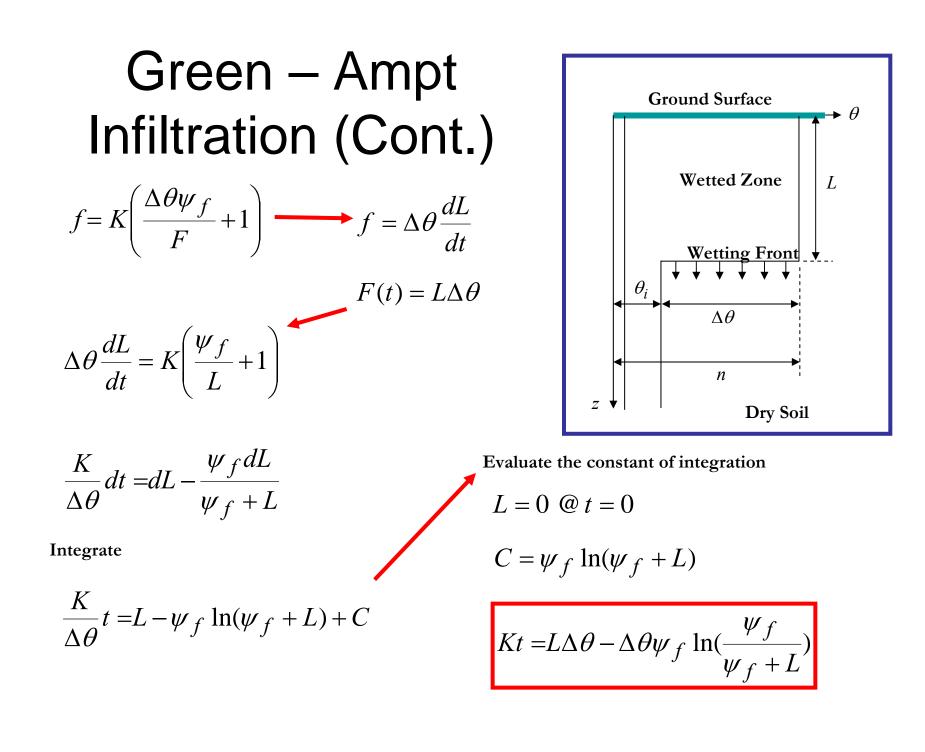
$$f = K \frac{\partial \psi}{\partial z} + K$$

- Apply finite difference to the derivative, between
 - Ground surface $z = 0, \psi = 0$
 - Wetting front $z = L, \psi = \psi_f$



$$f = K \frac{\partial \psi}{\partial z} + K = K \frac{\Delta \psi}{\Delta z} + K = K \frac{\psi_f - 0}{L - 0} + K$$

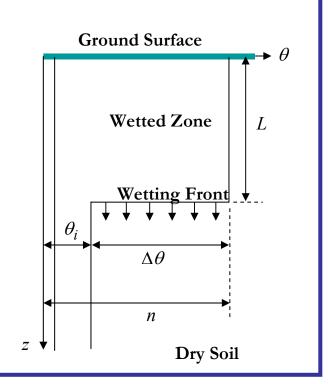
$$F(t) = L\Delta\theta$$
$$L = \frac{\Delta\theta}{F}$$
$$f = K \left(\frac{\Delta\theta\psi_f}{F} + 1\right)$$

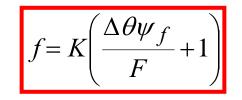


Green – Ampt Infiltration (Cont.)

$$Kt = L\Delta\theta - \Delta\theta\psi_f \ln(\frac{\psi_f}{\psi_f + L})$$

$$F = Kt + \Delta\theta\psi_f \ln(1 + \frac{F}{\Delta\theta\psi_f})$$





Nonlinear equation, requiring iterative solution.

See: <u>http://www.ce.utexas.edu/prof/mckinney/ce311k/Lab/Lab8/Lab8.html</u> And: <u>http://www.ce.utexas.edu/prof/mckinney/ce311k/homework/Solutions-F06/Lab8.pdf</u>

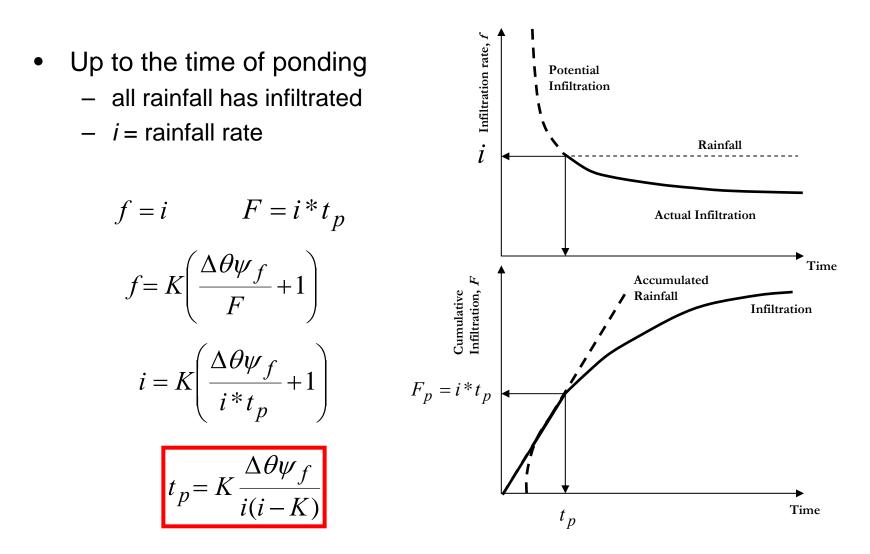
Soil Parameters

- Green-Ampt model requires
 - Hydraulic conductivity
 - Porosity
 - Wetting Front Suction Head

Soil Class	Porosity	Effective Porosity	Wetting Front Suction Head	Hydraulic Conductivity
	n	$ heta_e$	ψ	K
			(cm)	(cm/h)
Sand	0.437	0.417	4.95	11.78
Loam	0.463	0.434	9.89	0.34
Clay	0.475	0.385	31.63	0.03

$$\theta_e = n - \theta_r$$
 $\Delta \theta = (1 - s_e)\theta_e$ $s_e = \frac{\theta - \theta_r}{\theta_e}$

Ponding Time



Example

- Silty-Loam soil
- 30% effective saturation
- 5 cm/hr rainfall intensity

 $\theta_e = 0.486$ $\psi = 16.7 \, cm$ $K = 0.65 \, cm / hr$ $s_e = 0.30$

$$\begin{split} \Delta\theta &= (1 - s_e)\theta_e = (1 - 0.3)(0.486) = 0.340\\ \psi\Delta\theta &= 16.7*0.340\\ t_p &= K \frac{\Delta\theta\psi_f}{i(i - K)} = 0.65 \frac{5.68}{5.0(5.0 - 0.65)(i - K)} = 0.17\,\mathrm{hr} \end{split}$$